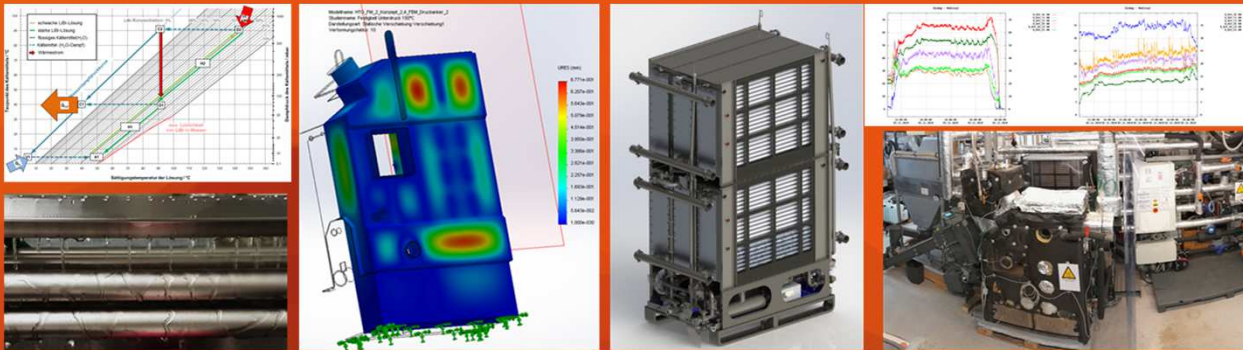


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# Two-stage biomass-fired absorption heating and cooling system

Manuel KAUSCHE,  
Martin Helm, Manuel Riepl, Wolfgang Aich





# Two-stage biomass-fired absorption heating and cooling system

## AGENDA:

Advantages of biomass directly fired AHP's

System concept and test-rig setup

Test results for highly efficient double effect mode

Outlook



Gefördert durch:



Bundesministerium  
für Wirtschaft  
und Klimaschutz

aufgrund eines Beschlusses  
des Deutschen Bundestages

Manuel KAUSCHE,

Martin Helm, Manuel Riepl, Wolfgang Aich



# Advantages of a two-stage heating and cooling system with directly fired biomass-combustion



- Potential of (ligneous) biomass is big, but limited, *utilisation of wood: “Building Construction FIRST!”*
- Heat from **biomass reliefs el. grids** and enables usage of wastewood
- Standardised, **storable** fuel and technically mature combustion: **wood chips or pellets**
- **Multistage = Flexibility** → in operation modes → temperatures → applications!

➔ **higher efficiency = less global warming!** (*and: consider refrigerants...*)

working pair: lithiumbromide and water

	biomass boiler	biomass boiler & single effect (SE)	biomass directly fired double effect (DE)
$BUE_h$	0,9	1,5	2,0

“DE, 1 MW? Buy it!”

“DE, 100 kW??!  
To be developed...”

$$BUE_h = \text{Biomass Utilization Efficiency "heat"} = \frac{\text{heat}}{\text{fuel energy}}$$

## Modelling of the heating and cooling system

### engineering guideline

- economic and reliable, capacity-class: 100 kW
- producable with common fabrication methods of boiler manufacturers
- cubic “europalett“-design of main components

### guiding design temperatures

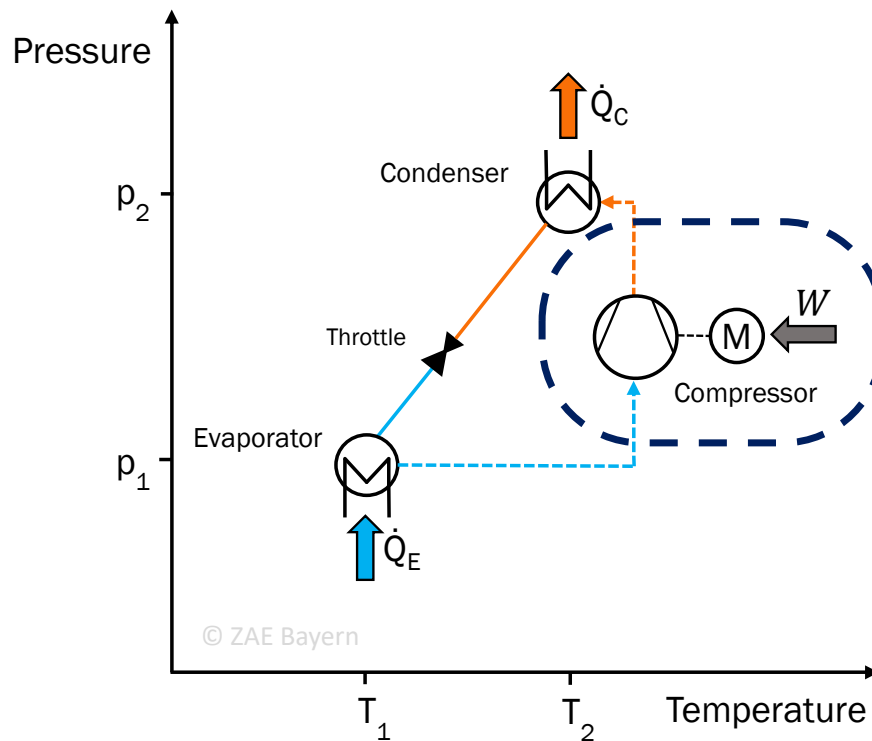
- choosen for application as a **double effect heat pump**
  - ✓ ambient heat source **4|8 °C** (groundwater, wastewater, geoth.probes, ...)
  - ✓ heat for new-building standards **41|31 °C** (e.g. floor heating)

### Modular system setup

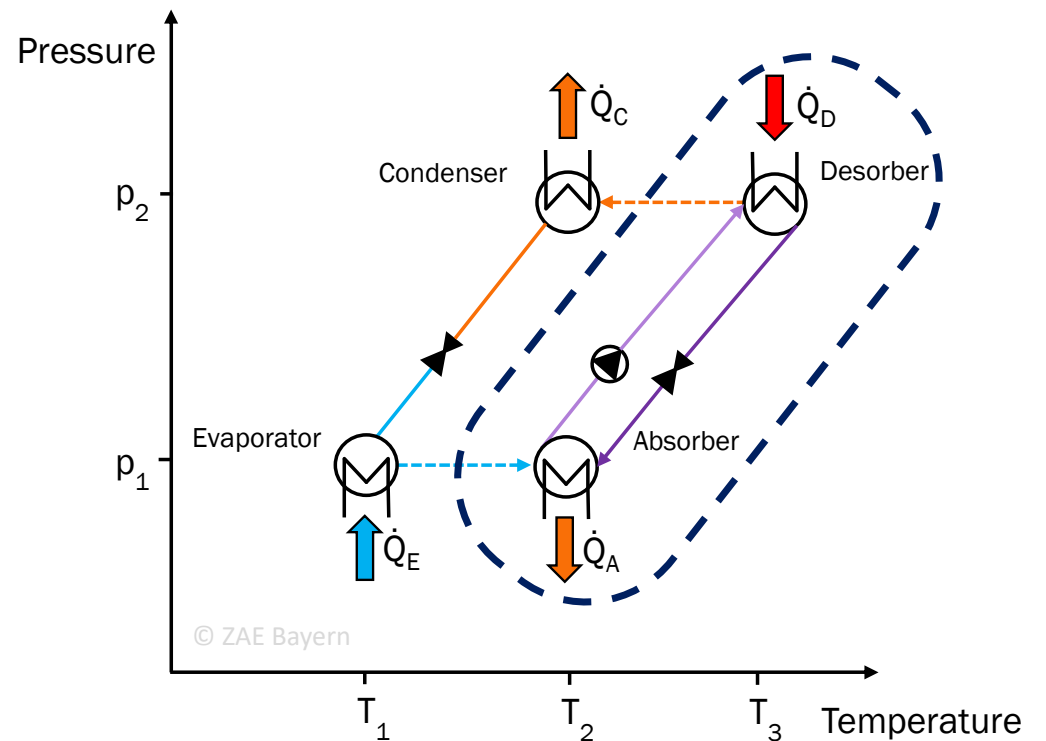
- The choosen design and plug&play hydraulic system enables
  - ✓ **Easy insertion as well as error-free installation and integration into buildings or quarters.**
  - ✓ **Coupling of e.g. solar thermal or other waste heat for cooling (summer!),**  
*but also heat pump drive (winter!)*
  - ✓ **Wells or geoth. probes as well as geothermal energy (as ambient heat source ) enable additional, fuel-free cooling**

# Operating principles of the drive types commonly used for heat pumps and cooling systems

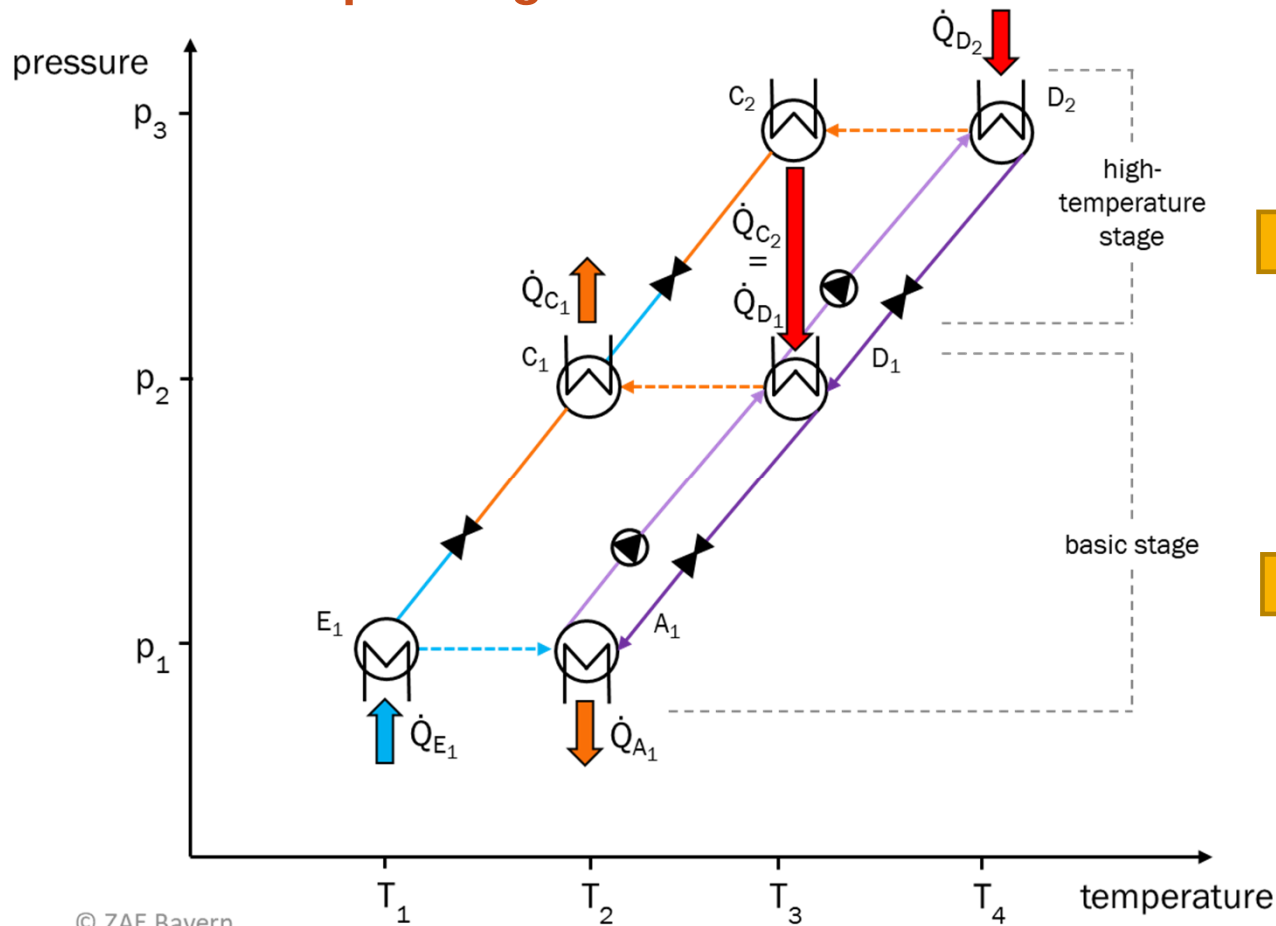
*elektromechanical drive*



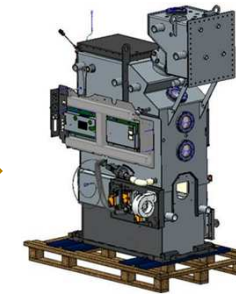
*thermal drive*



# Highly efficient, two-stage absorption heat pump process in schematic p-T-diagram



Hightemperature desorber (HTD)

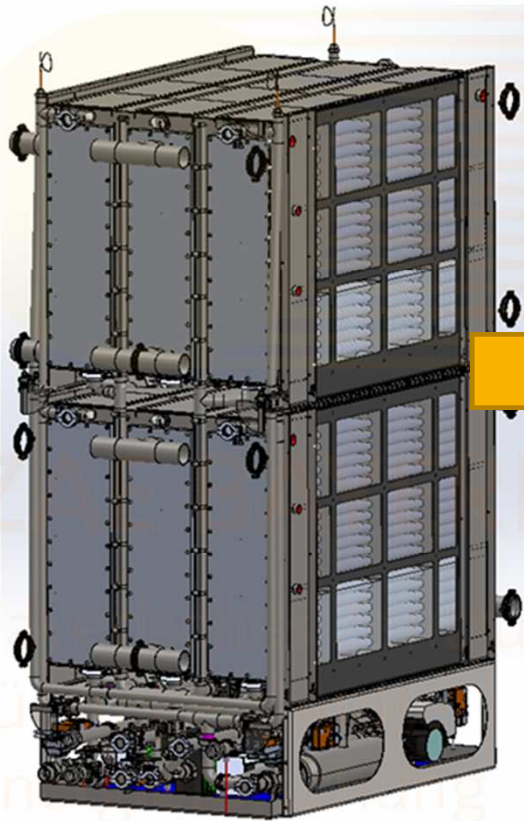


Single-stage "absorption heat pump" (AHP) designed as a tube bundle

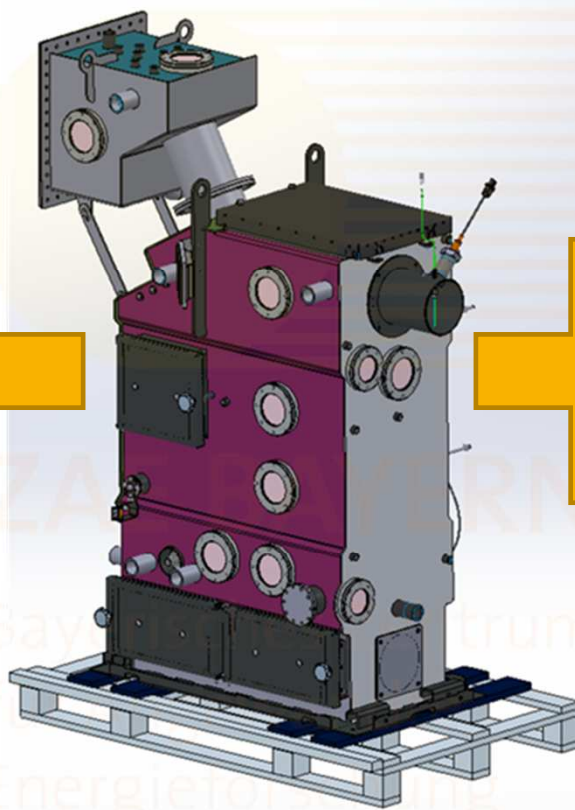


# Developed plant and test-rig setup

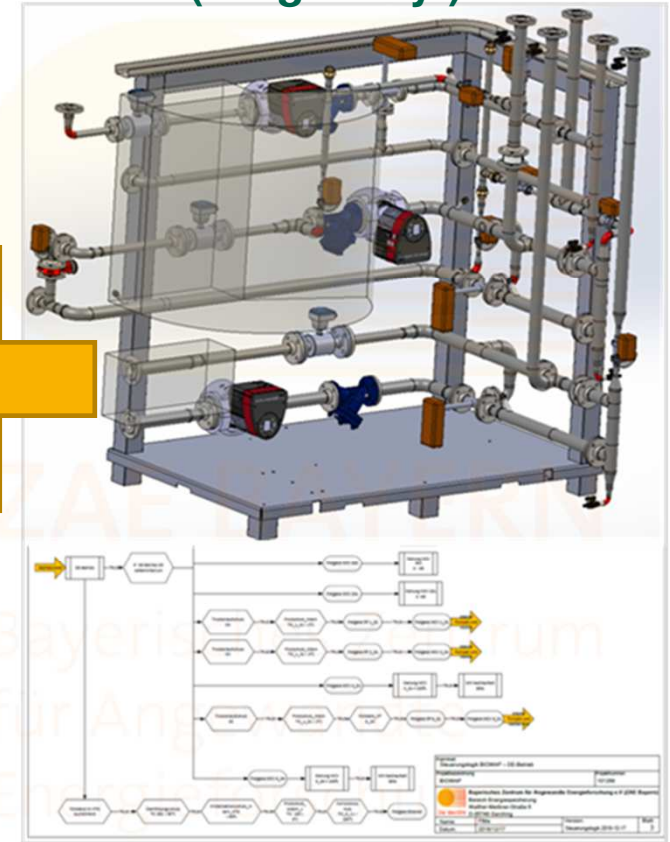
**Absorption Heat Pump (AHP)**



**High Temperature Desorber (HTD)**



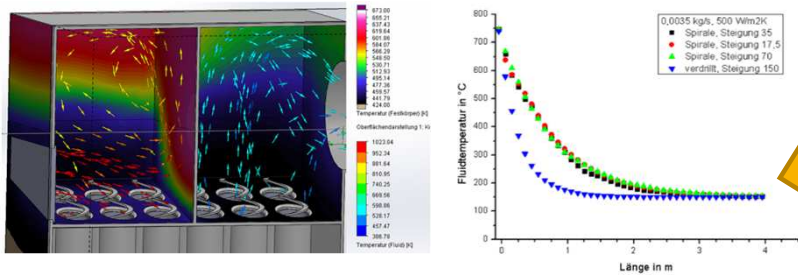
**Hydraulics & Control (Plug&Play)**



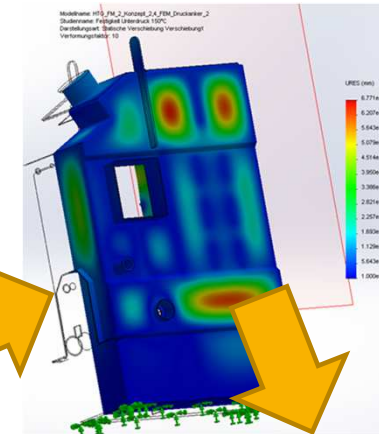
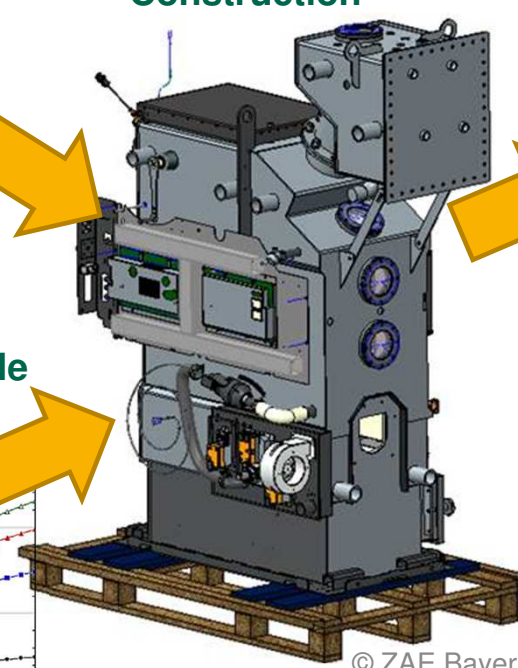
# Core piece: wood-pellets-directly-fired High Temperature Desorber (HTD)

## Stress analysys

## Heat transfer fluegas-side



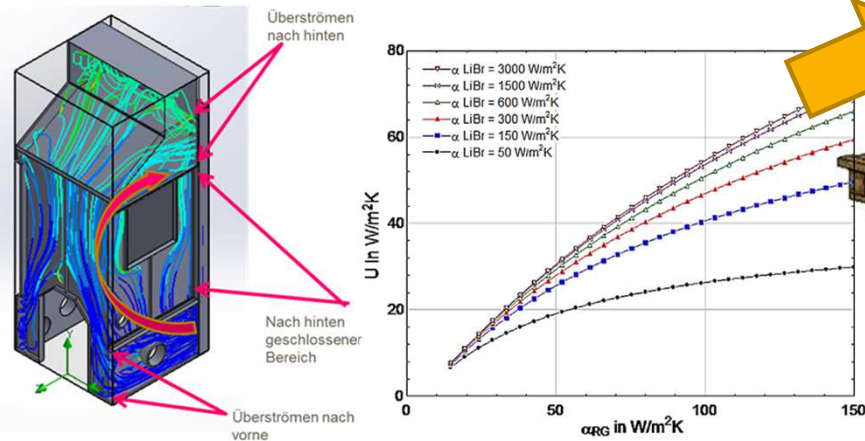
## Construction



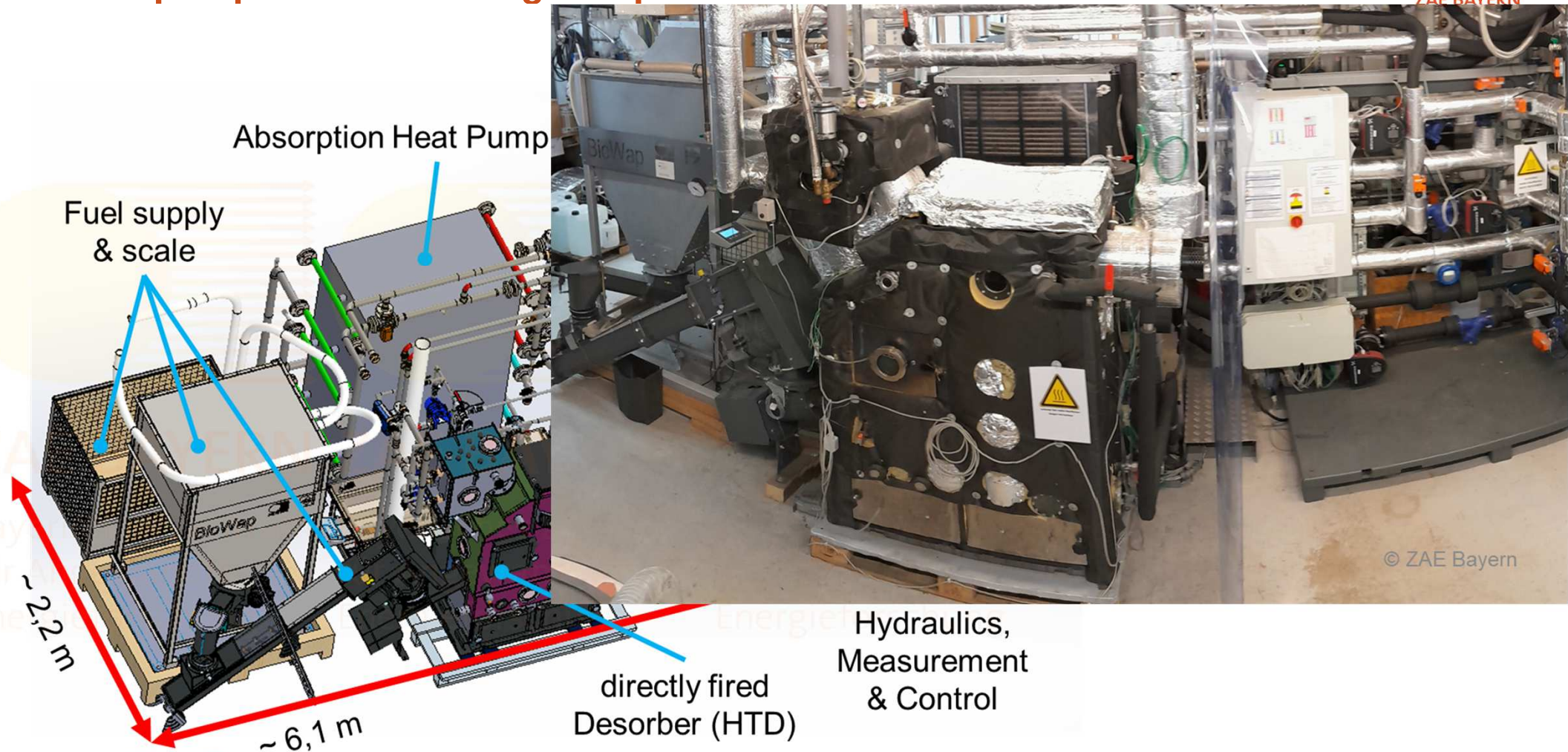
## Fabrication



## Natural convection & heat transfer solution-side

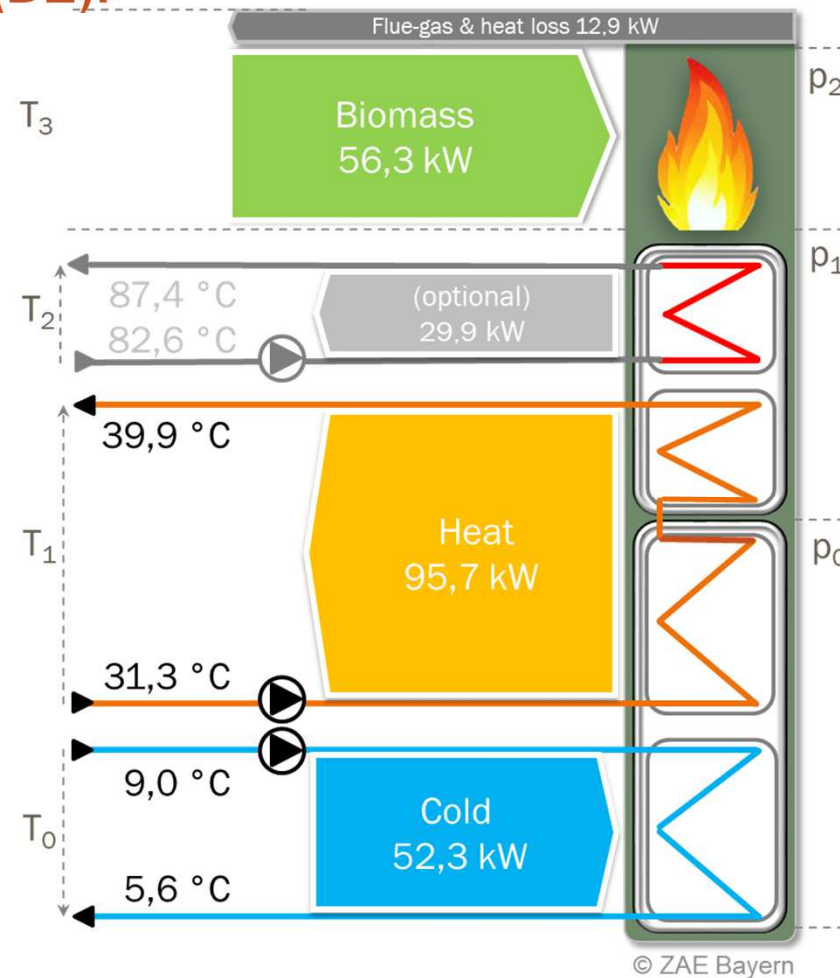
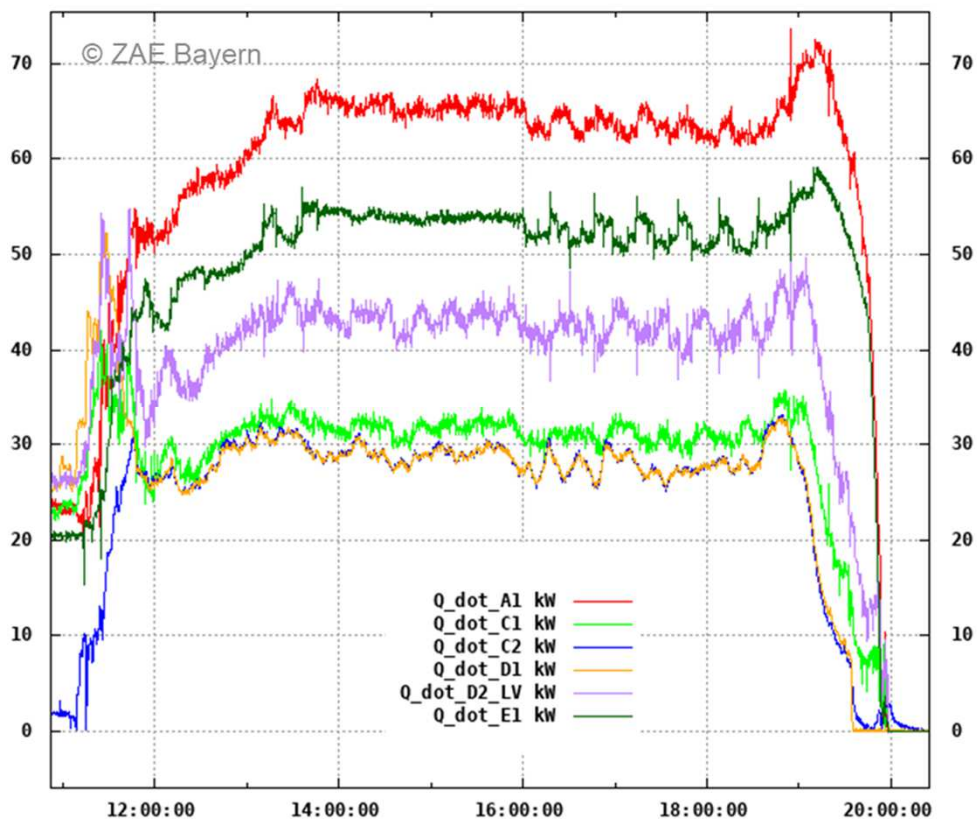


# Developed plant and test-rig setup

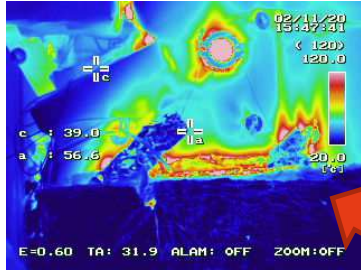
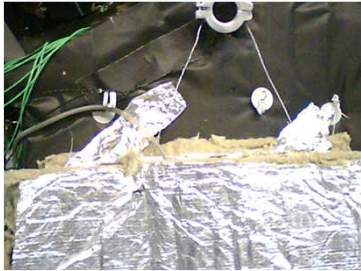


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## Test results for the double effect mode (DE):



# Thermal losses lower the performance significantly – example from the double effect results:



➤ Thermal losses caused by the measurement setup lowers  $\dot{Q}_{HTD}$ , therefore  $\eta_{HTD}$  and  $BUE_h$ .

## Process based figure:

$$\zeta_{heat} = 2,2$$

$$\frac{\text{heat}}{\text{driving heat } (\dot{Q}_{HTD})}$$

## Fuel based figures:

$$\eta_{HTD} = 77 \%$$

$$\frac{\text{driving heat } (\dot{Q}_{HTD})}{\text{fuel energy}}$$

## Biomass Utilization Efficiency “heat”

$$BUE_h = 1,7$$

$$\frac{\text{heat}}{\text{fuel energy}}$$

	Simulation	Test result	Uncertainty
$T_{cold} \text{ (supply)}$	4 °C	5,6 °C	±0,10 K
$T_{cold} \text{ (return)}$	8 °C	9,0 °C	±0,09 K
$T_{heat} \text{ (supply)}$	41 °C	39,9 °C	±0,17 K
$T_{heat} \text{ (return)}$	31 °C	31,3 °C	±0,19 K
$T_{lift}$	37 K	34,4 K	±0,19 K
$\dot{Q}_{E1}$	61,5 kW	52,3 kW	±2,10 kW
$\dot{Q}_{A1}$	77 kW	64,1 kW	±2,86 kW
$\dot{Q}_{C1}$	34,1 kW	31,6 kW	±2,65 kW
	33,6 kW	29,9 kW	±2,21 kW
$\dot{Q}_{C2}$	33,6 kW	29,9 kW	±2,58 kW
$\dot{Q}_R$	111,1 kW	95,7 kW	±3,90 kW
$\dot{Q}_{HTD}$	50 kW	43,4	±3,35 kW
$\zeta_{cold}$	1,23	1,21	±0,01
$\zeta_{heat}$	2,22	2,21	±0,12
$\dot{Q}_B$	56,8 kW	56,3	±0,30 kW
$T_{Ac}$	-	189,8 °C	±4,19 K
$\eta_{HTD}$	88 %	77 %	±6,2 %
$EEH$	-	03,4	±2,89
$CO_2$	-	152,1	±4,83
$BUE_h$	1,96	1,70	±0,07
$BUE_c$	1,08	0,93	±0,04

## Conclusions and outlook

*the directly biomass-fired absorption heat pump system for capacities around 100 kW...*

- ✓ is technically **feasible**, whilst **economically justifiable**
- ✓ **doubles the heat-output & halves emissions** compared to conventional bio-boilers
- ✓ enables upgrading **low temperature heat** reservoirs **at ~ 4 °C**
- ✓ **suits** especially to **medium-sized enterprises** or **residential areas**
- ✓ highly efficient **converts** (waste-) **biomass** energy into useable cold **for cooling**
- ✓ as a **“two-stager”** enables multiple modes of operation: **DE, DL, DE/SE, ...**

*... prospective work:*

- ❖ system optimization and pilot plants
- ❖ further applications such as extracting heat from flue gas by condensing
- ❖ Scientific discussion!

**BioWap at a glance:**

- Combustion capacity ~ 55 kW
- Heating capacity ~ 111 kW
- Cooling capacity ~ 62 kW
- Temperatures ~ 4/8 & 31/41 °C up to 95 °C

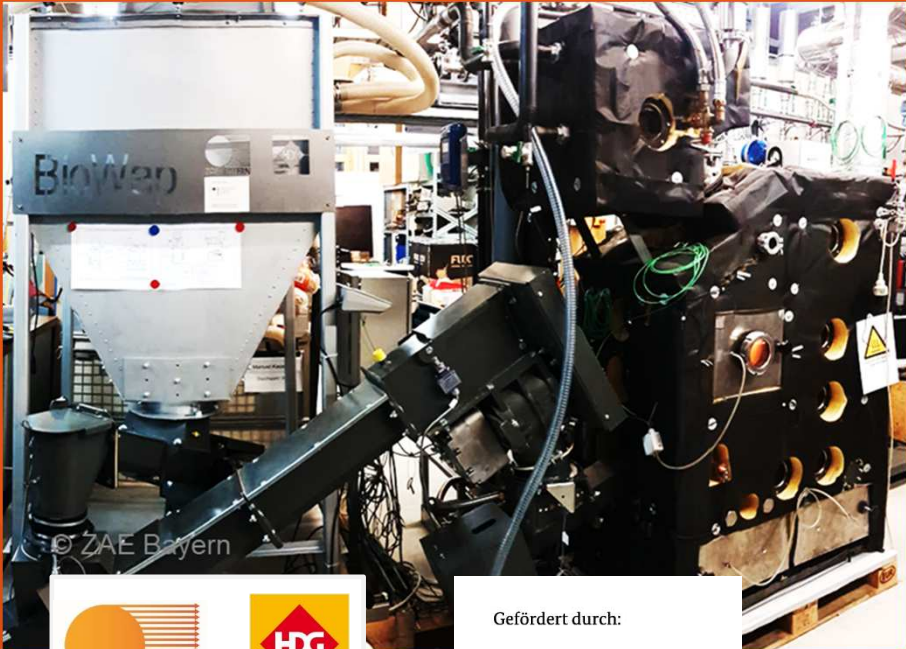
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Project BioWap



FKZ 03KB127

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für Wirtschaft  
und Klimaschutz

aufgrund eines Beschlusses  
des Deutschen Bundestages

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# Efficiency lead – conventional systems vs. BioWap:

**conventional:**

$$BUE_h = \frac{\dot{Q}_{heat}}{H_i \cdot \dot{m}_B} \approx 1,56$$

$$\eta_B = \frac{\dot{Q}_{D1}}{H_i \cdot \dot{m}_B} \approx 0,91$$

$$\zeta_{SE,heat} = \frac{\dot{Q}_{heat}}{\dot{Q}_{D1}} \approx 1,72$$



Pelletboiler



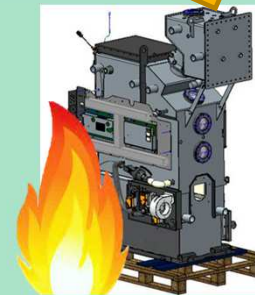
AHP

**BioWap:**

$$BUE_h = \frac{\dot{Q}_{heat}}{H_i \cdot \dot{m}_B} \approx 1,96$$

$$\eta_{HTD} = \frac{\dot{Q}_{D2}}{H_i \cdot \dot{m}_B} \approx 0,88$$

$$\zeta_{DE,heat} = \frac{\dot{Q}_{heat}}{\dot{Q}_{D2}} \approx 2,23$$



High temperature desorber (HTD)



AHP